

# Critical Evaluation and Optimization of the Fe-Nb-N System



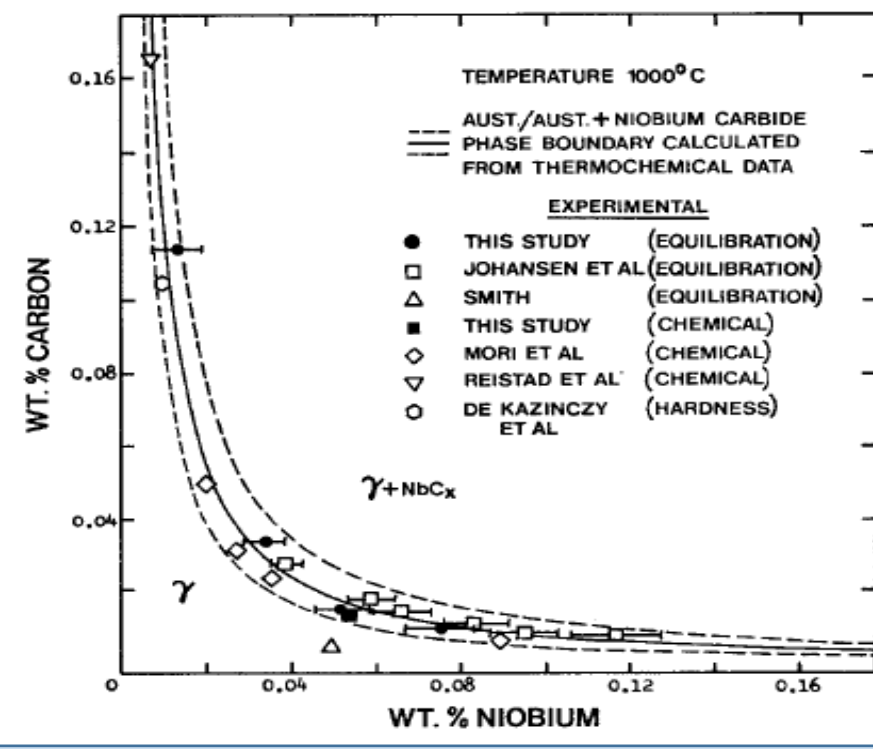
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## Introduction

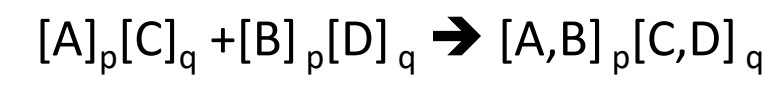
### Niobium Nitride

- Main strengthening element for commercial steel & hard coating materials
- Enables High strength Low Alloy steel(HSLA) to be resistant to corrosion



## Model

- Solid solution (Compound Energy Formalism)



$$G_M = y_A y_C g_{AC}^0 + y_A y_D g_{AD}^0 + y_B y_C g_{BC}^0 + y_B y_D g_{BD}^0 + pRT(y_A \ln y_A + y_B \ln y_B) + qRT(y_C \ln y_C + y_D \ln y_D) + G^{XS}$$

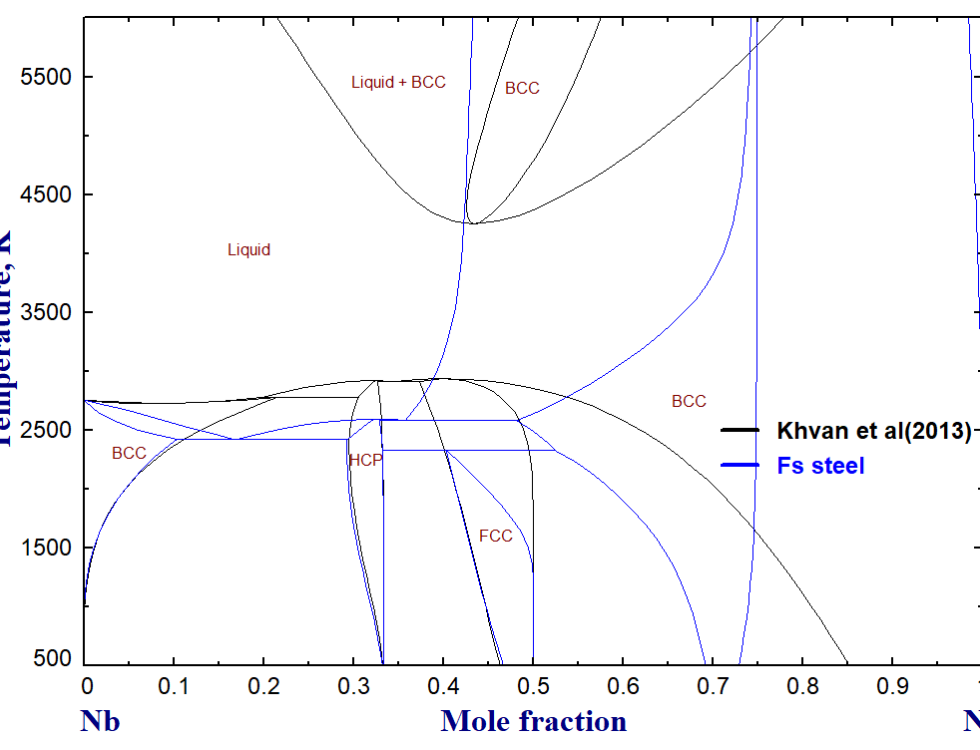
- Liquid solution (Modified Quasichemical Model)

$$G^m = (n_i g_i^0 + n_j g_j^0) - RT \Delta S^{\text{config}} + \left(\frac{n_i - j}{2}\right) \Delta g_{i-j}$$

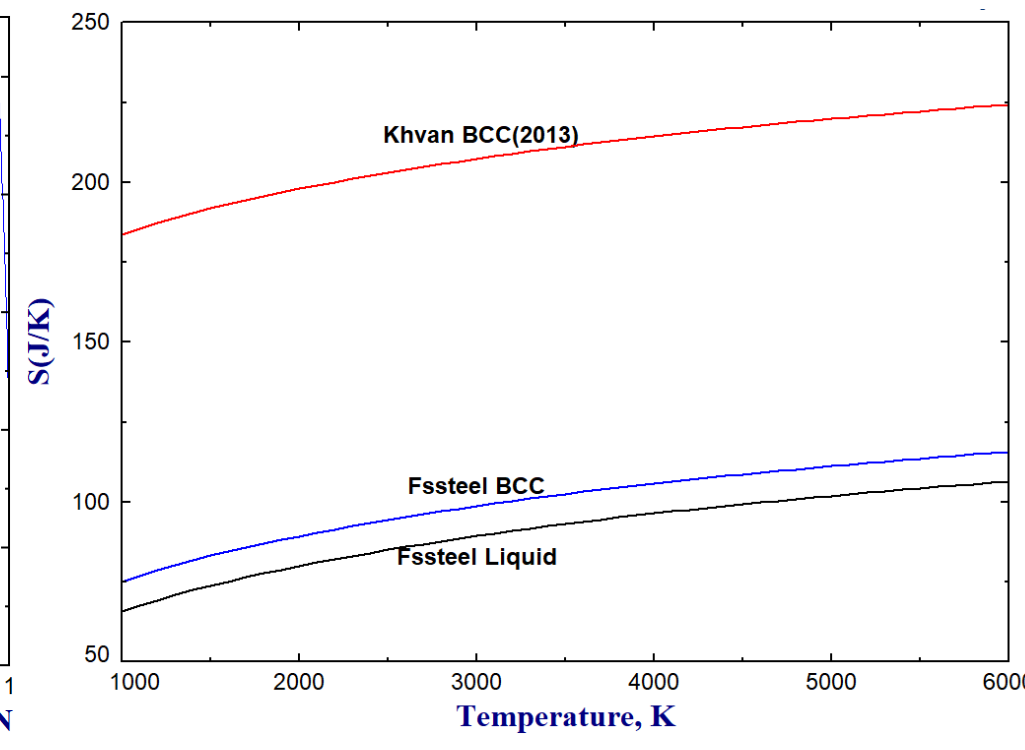
$$\Delta g_{i-j} = \Delta g_{i-j}^{00} + \sum q_{ij}^{mn} X_{ii}^m X_{jj}^n$$

## Main Issue

### Bcc Intrusion issue

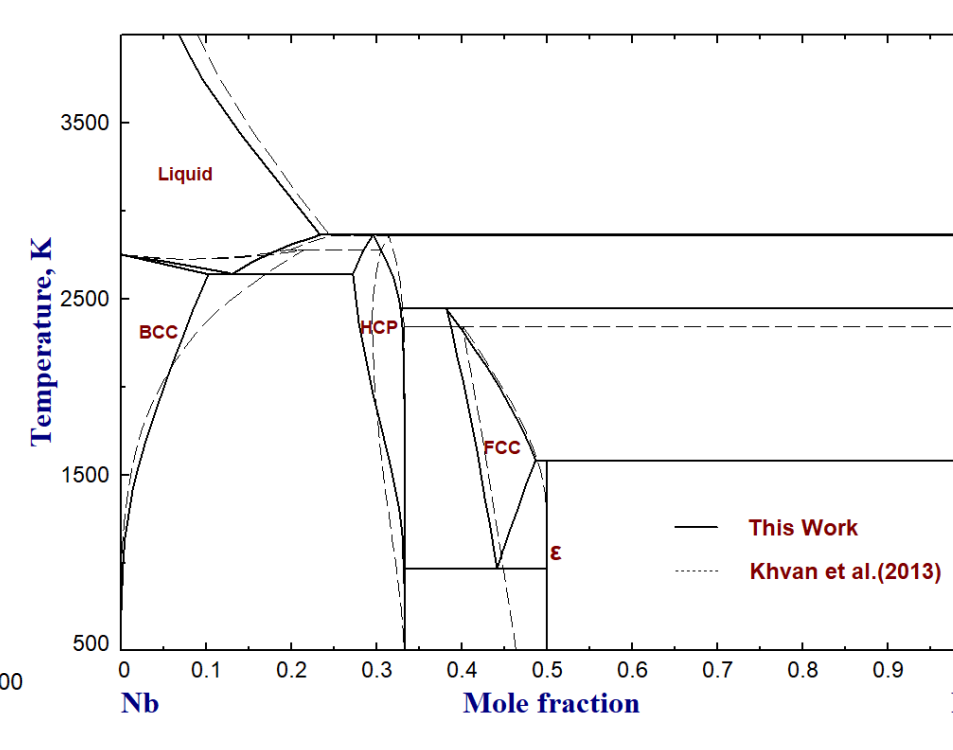


Gas suppressed condition

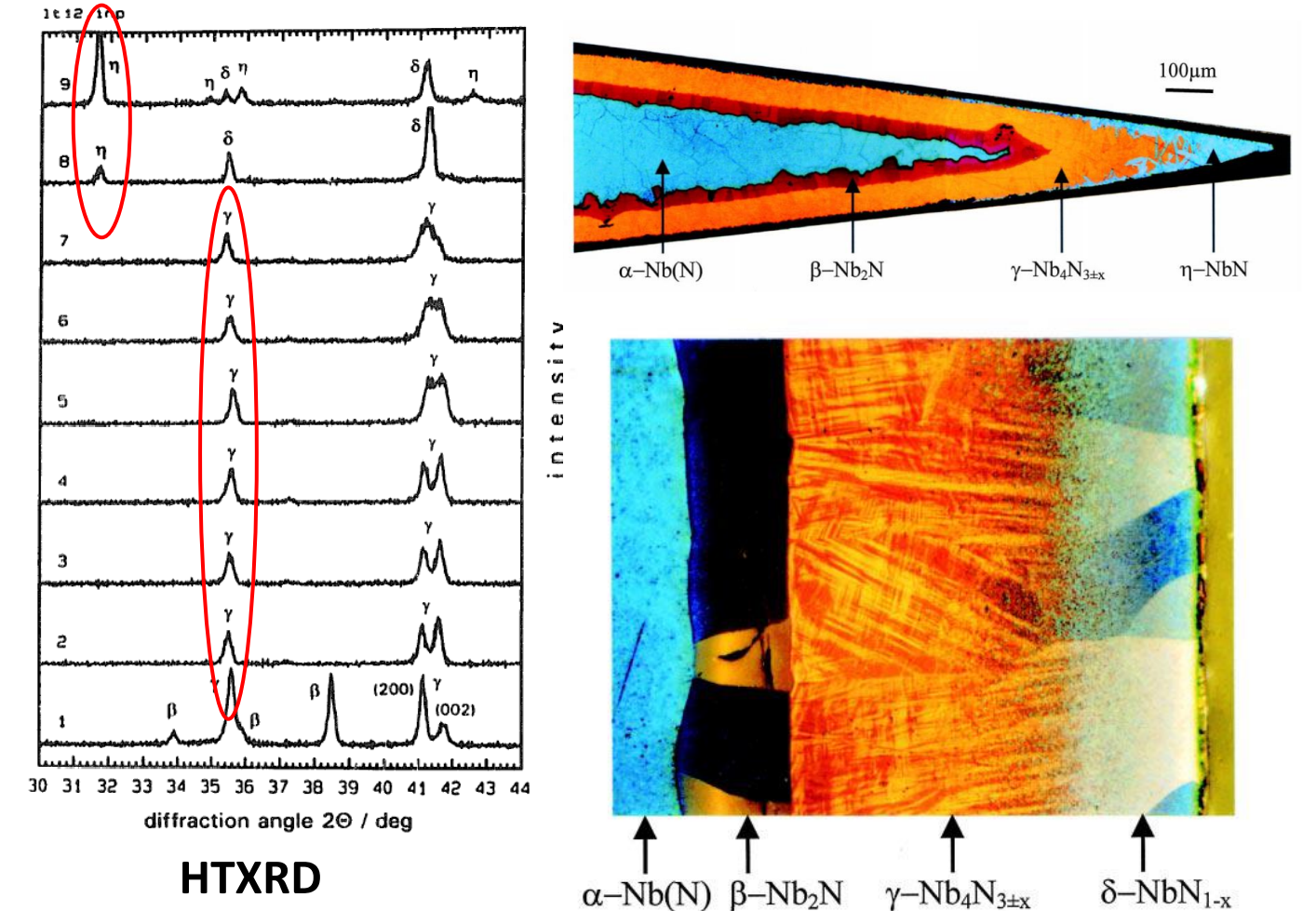


Entropy of Bcc and Liquid phase

### Stable phase issue



Stable phase modification

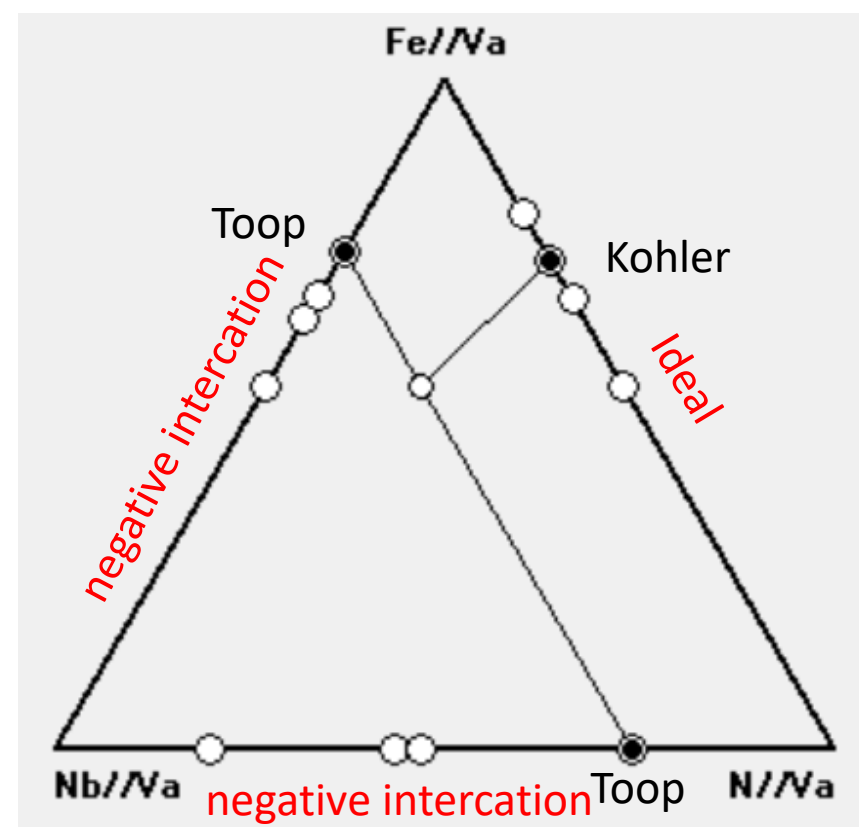


## Model Parameters

### End members

- Liquid (Modified Quasichemical Model)
- Non default Quadruplet
- $Z_{Fe}^{Fe} = 6, Z_{Nb}^{Nb} = 4, Z_{Fe}^{Nb} = 4, Z_{Nb}^{Fe} = 6$
- Kohler/Toop interpolation - Nb asymmetric

$$\begin{aligned} \Delta g_{FeNb}^{00} &: -15100 + 4.9624T \\ q_{FeNb}^{10} &: 4100 - 4.6878T \\ q_{FeNb}^{01} &: -14900 + 5.4378T \\ \Delta g_{NbN}^{00} &: -46247 - 1.203T \\ q_{NbN}^{10} &: -27625 + 10.9375T \\ q_{NbN}^{01} &: -62041 + 17T \end{aligned}$$



- BCC** :  $(Fe,Nb)_1(N,Va)_3$ 

$$\begin{aligned} G_{FeVa}^{BCC} &= G_{Fe}^0(BCC) \\ G_{NbVa}^{BCC} &= G_{Nb}^0(BCC) \\ G_{FeN}^{BCC} &= G_{Fe}^0(BCC) + 3G_{N}^0(BCC) + 61418 \\ G_{NbN}^{BCC} &= G_{Nb}^0(BCC) + 3G_{N}^0(BCC) + 29028 - 31.75 \\ L_{BCC}^{0FeNbVa} &= -5950 + 9.4T \\ L_{BCC}^{0FeNbVa} &= 14000 - 13.96T \\ L_{BCC}^{0NbN} &= -660784 + 120T \\ TC_{FeVa} &= 1043, \beta_{FeVa} = 2.22 \end{aligned}$$
- FCC** :  $(Fe,Nb)_1(N,Va)_1$ 

$$\begin{aligned} G_{FeVa}^{FCC} &= G_{Fe}^0(FCC) \\ G_{NbVa}^{FCC} &= G_{Nb}^0(FCC) + 13500 + 1.7T \\ G_{FeN}^{FCC} &= G_{Fe}^0(FCC) + G_{N}^0(FCC) - 22361 + 30T \\ G_{NbN}^{FCC} &= G_{Nb}^0(FCC) + G_{N}^0(FCC) - 22919 + 30T \\ L_{FCC}^{0FeNbVa} &= 7740 - 11.4T \\ L_{FCC}^{0FeNbVa} &= -7041.7 - 15.3553T \\ L_{FCC}^{0NbN} &= -67500 \\ TC_{FeVa} &= -201, \beta_{FeVa} = 2.22 \\ TC_{NbN} &= -201, \beta_{NbN} = 2.22 \end{aligned}$$
- Mu** :  $(Fe)_1(Fe,Nb)_2(Nb)_4(Fe,Nb)_6$ 

$$\begin{aligned} G_{FeFeNbFe}^{Mu} &= 9G_{Fe}^0(BCC) + 4G_{Nb}^0(BCC) - 138800 \\ G_{FeFeNbNb}^{Mu} &= 3G_{Fe}^0(BCC) + 10G_{Nb}^0(BCC) + 850000 \\ G_{FeNbNbFe}^{Mu} &= 7G_{Fe}^0(BCC) + 6G_{Nb}^0(BCC) - 248480 + 60.9T \\ G_{FeNbNbNb}^{Mu} &= G_{Fe}^0(BCC) + 12G_{Nb}^0(BCC) + 150000 \end{aligned}$$
- Hcp** :  $(Fe,Nb)_1(N,Va)_{0.5}$ 

$$\begin{aligned} G_{FeVa}^{HCP} &= G_{Fe}^0(HCP) \\ G_{NbVa}^{HCP} &= G_{Nb}^0(BCC) + 10000 + 2.4T \\ G_{FeN}^{HCP} &= G_{Fe}^0(HCP) + 0.5G_{N}^0(HCP) - 17865 + 8.71T \\ G_{NbN}^{HCP} &= G_{Nb}^0(BCC) + 0.5G_{N}^0(HCP) - 134800 + 12T \\ L_{HCP}^{0FeNbVa} &= 15255 - 26.359T \\ L_{HCP}^{0FeNbVa} &= -16840 + 16.8824T \\ L_{HCP}^{0NbN} &= 18600 - 10T \end{aligned}$$
- C14** :  $(Fe,Nb)_2(Fe,Nb)_1$ 

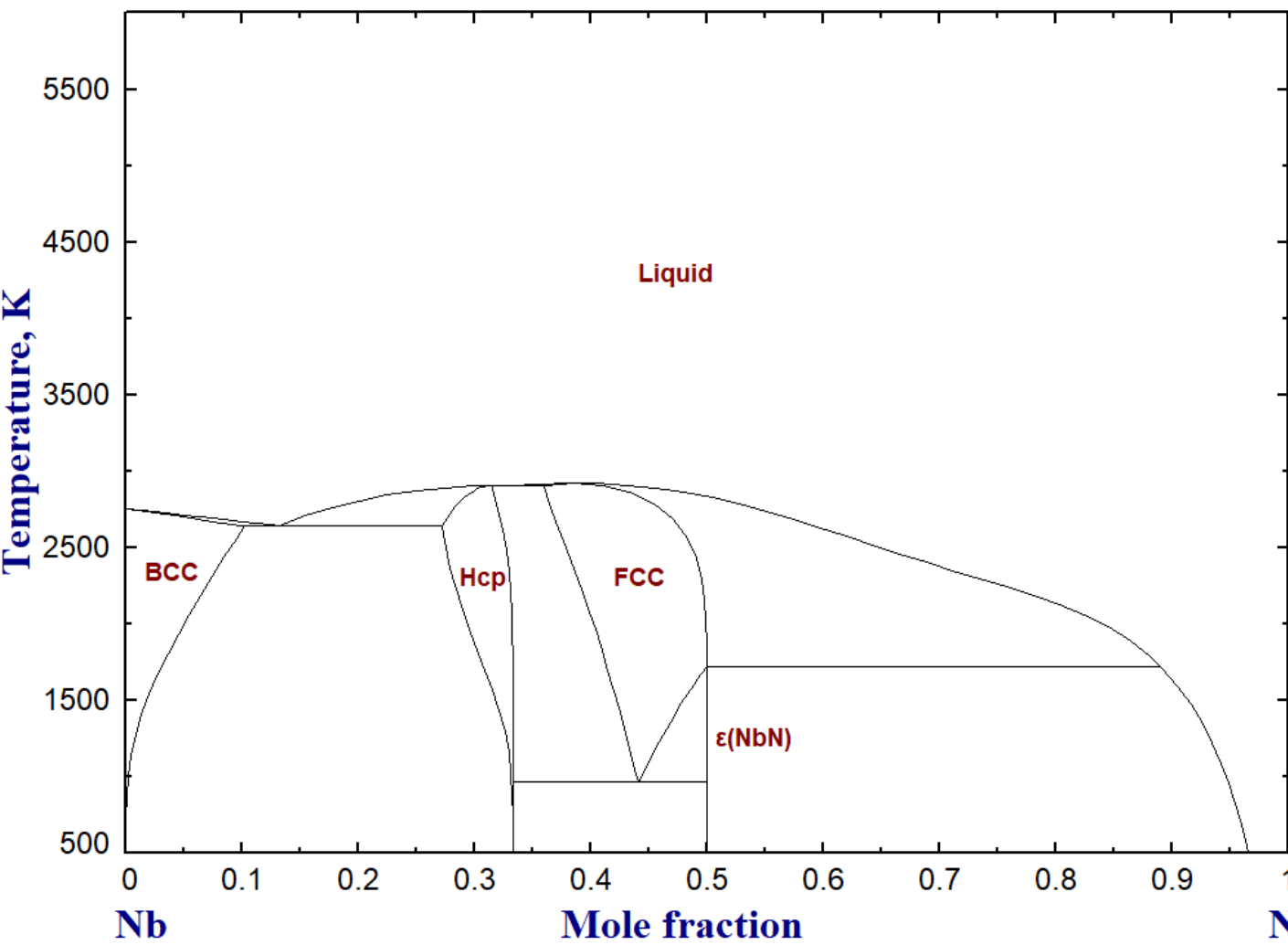
$$\begin{aligned} G_{FeFe}^{C14} &= 3G_{Fe}^0(BCC) + 51292 - 5T \\ G_{FeNb}^{C14} &= 2G_{Fe}^0(BCC) + G_{Nb}^0(BCC) - 61732 + 12.9T \\ G_{NbFe}^{C14} &= G_{Fe}^0(BCC) + 2G_{Nb}^0(BCC) + 90000 \\ G_{NbNb}^{C14} &= 3G_{Nb}^0(BCC) + 46110 \\ L_{C14}^{0FeFeNb} &= -59320 + 13T \\ L_{C14}^{0FeNbNb} &= 32000 \end{aligned}$$
- Gamma** :  $(Fe)_4(N,Va)_1$ 

$$\begin{aligned} G_{FeN}^{Gamma} &= 4G_{Fe}^0(FCC) + G_{N}^0(Gamma) - 44439 + 14.3T \\ G_{FeVa}^{Gamma} &= 4G_{Fe}^0(FCC) + 200 \\ G_{FeNbVa}^{Gamma} &= 50446.5 = 23.6396T \\ L_{Gamma}^{0FeNb} &= -13388.8 \end{aligned}$$

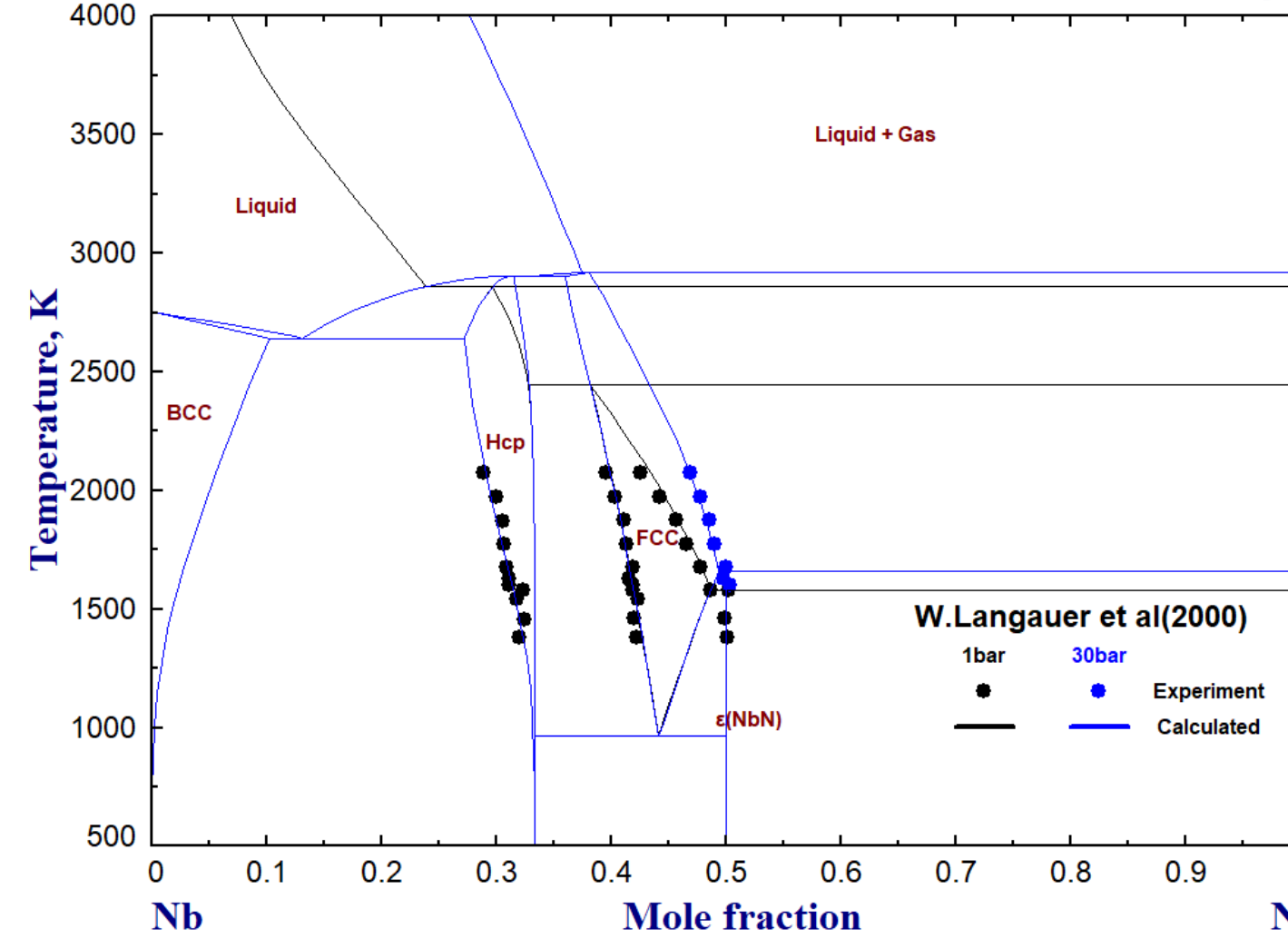
## Results & Discussion

### Fe-Nb-N phase diagram

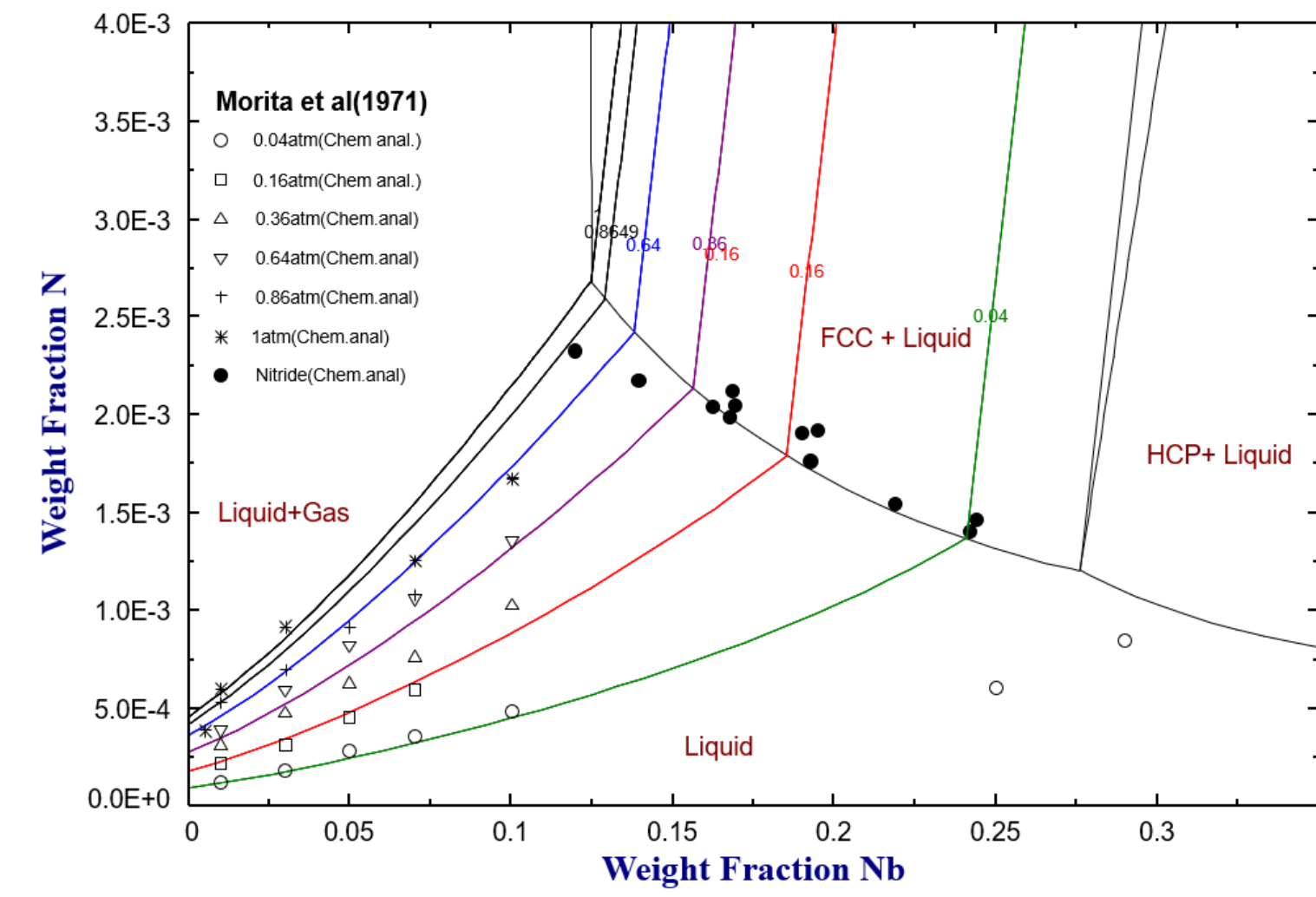
- Gas suppressed condition



### Binary phase boundary



### Ternary phase boundary (1923K)



## Conclusion

- Fe-Nb-N system was optimized
- Stable phase issue was addressed to determine  $\gamma, \epsilon$  phase as stable phases
- Bcc phase inclusion issue was addressed and solved using specific reference energy for each nitrogen phase
- Fe-rich ternary phase boundary could be properly expressed using Nb asymmetric Toop interpolation

## Future work

- Expand to Fe-Nb-C-N system to successfully express property of Carbonitrides in austenitic steel